



Natural external hazards, uncertainty and probability of exceedance hazard curves

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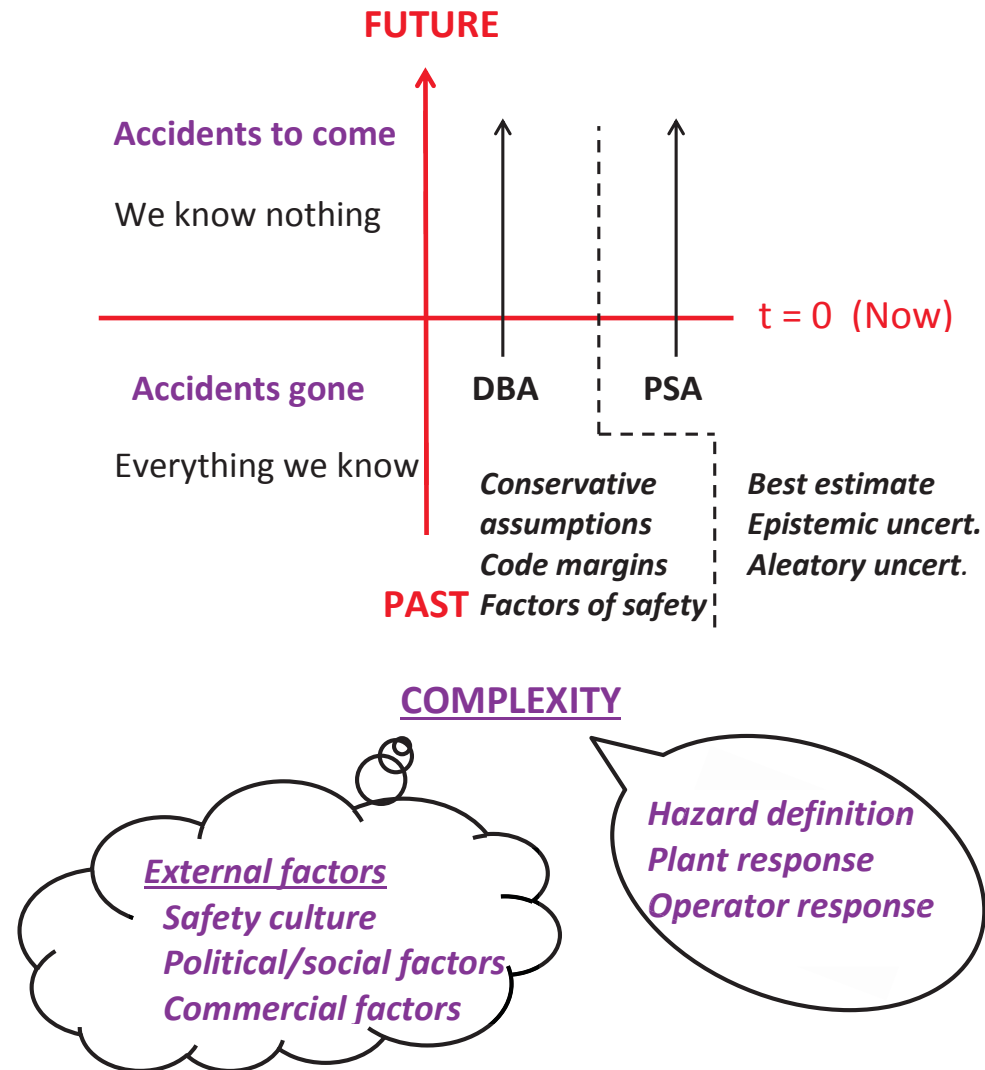
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- Characterising natural hazards
- Using a simple risk model to explore special features of natural hazards
 - Defining hazard across broad initiating frequencies range, rather than one discrete frequency
 - Common cause effect
 - Potential effect on overall plant risk
- Final thought!

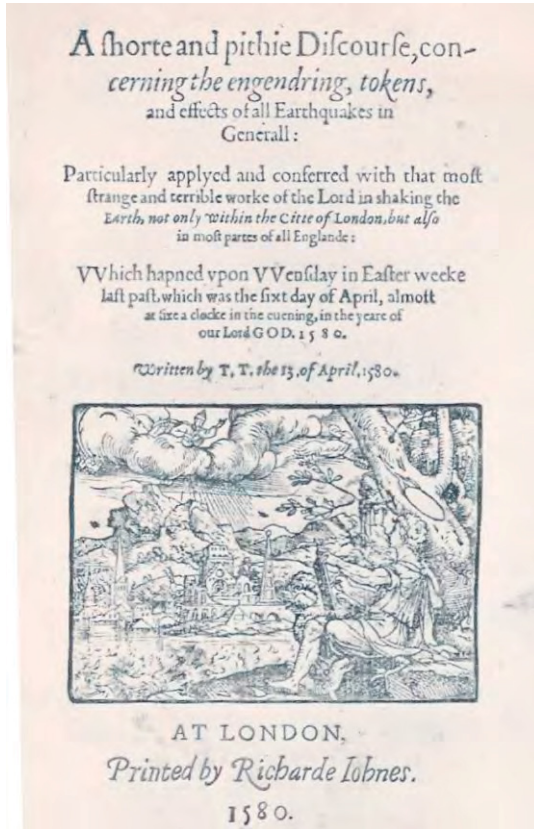
Origin of uncertainty



Characteristics of natural external hazards

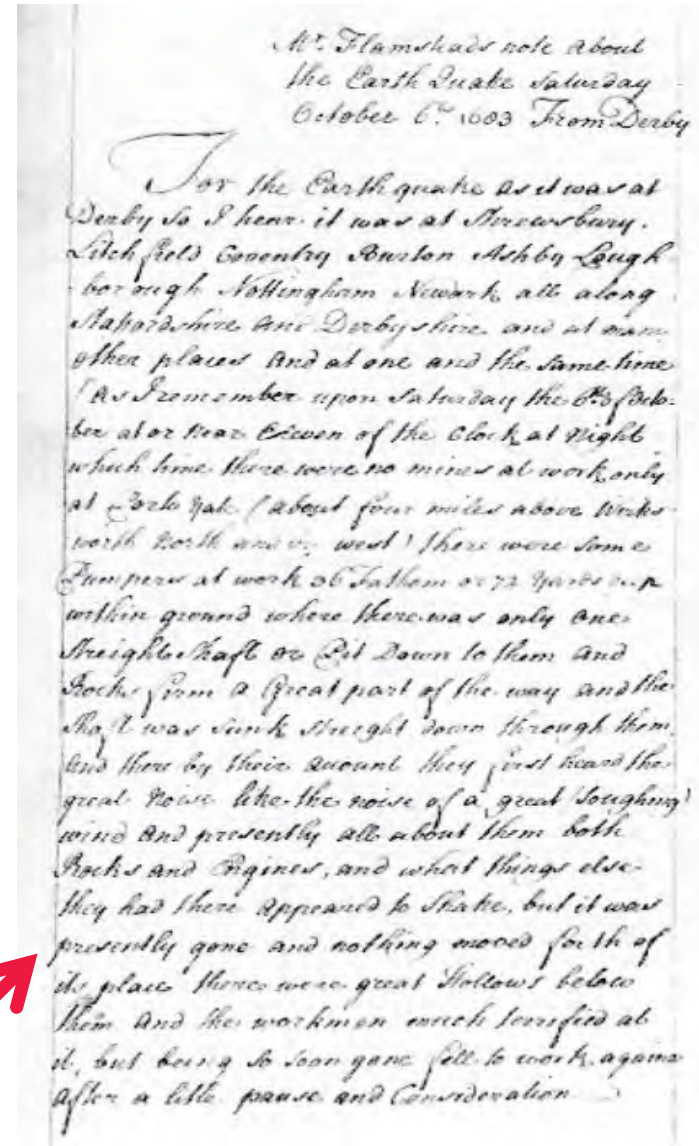
- Realised over a broad range of magnitudes/severities
- Complex physics
- Driven by conservation of energy on a planetary scale, modified by regional and very local effects
- Large uncertainties in ability to predict at site-specific scales and very low probabilities – 10^{-4} /yr and less
- Describing natural hazards
 - Hazard curve: Probability of exceedance v. hazard magnitude/severity
 - Plus more detailed descriptions for design purposes
- Quality of data
 - Instrumental (good / ~50yrs), Scientific, quantitative
 - historical (medium-poor / ~1000 yr, - drives seismic hazard at 10^{-4} /yr
 - Historical newspaper accounts, church records etc
 - Transcribed by interpretation into quantitative data
 - Geological (poor–very poor / ~ MA), Scientific, qualitative

Historical seismicity data - UK

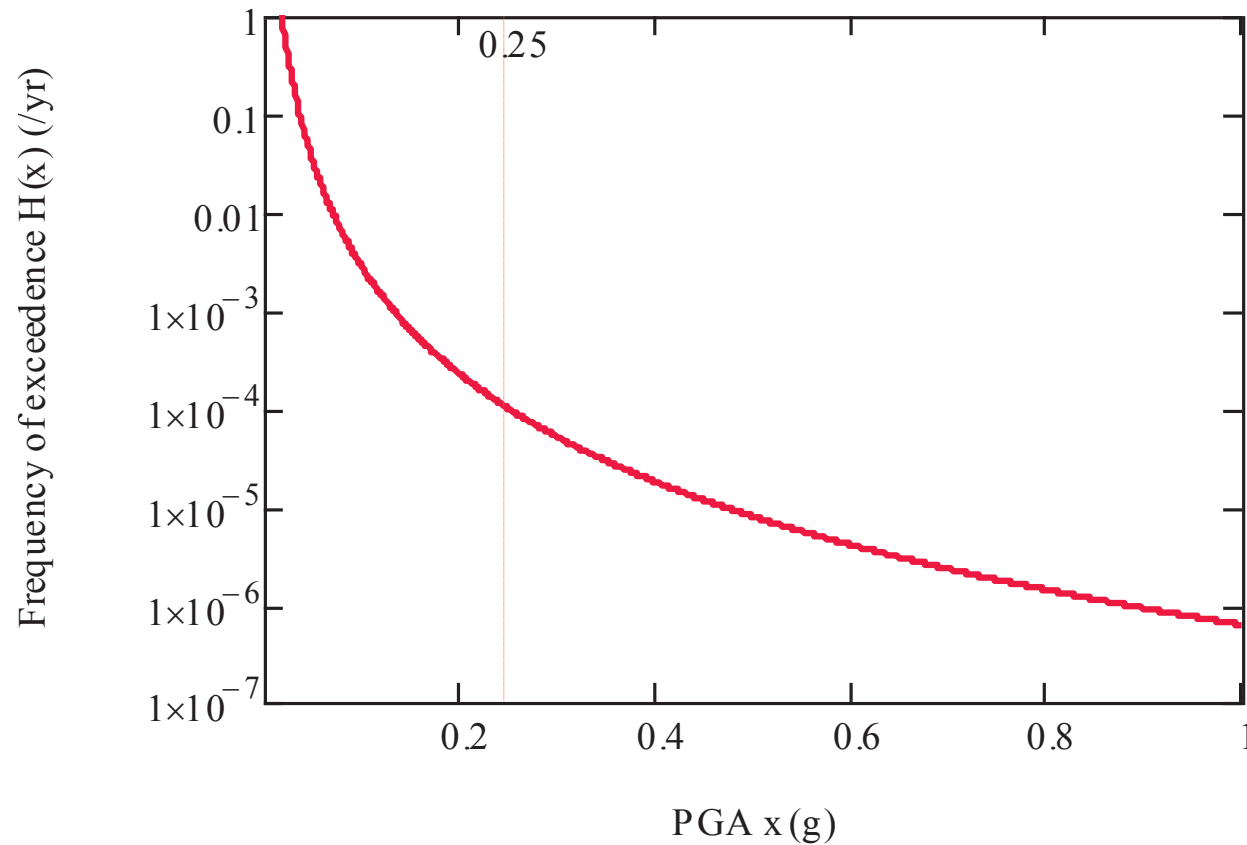


This was one of the largest and most damaging British earthquakes 6 April 1580

Letter referring to earthquake in Derbyshire, 6 October 1603



Typical hazard curve - seismic



Prob. of exceedance – seismic hazard

- A point on the hazard curve: “Probability of exceedance” v. “ X ” means (using $X = 0.25g$ as an example)
 - Prob ($x > 0.25g$) = $10^{-4}/\text{yr}$, or Prob ($0.25g < x < \infty$) = $10^{-4}/\text{yr}$
 - Where ∞ is a hazard magnitude for which plant has effectively no withstand capability and/or max. earthquake the geology can support
- If Design Basis is X_{DB} defined at $10^{-4}/\text{yr}$ hazard level
 - Why is X_{DB} normally defined as: $0.25g = x_{min}$?
 - Why not X_{DB} defined as: $\text{mean}(x)$?
- Exceedance probability hazard curves have implications for:
 - Importance of having a conservative plant design at Design Basis
 - Importance of Beyond Design Basis analysis
 - Ability of designers to control hazard induced plant risk

Plant risk from natural hazards

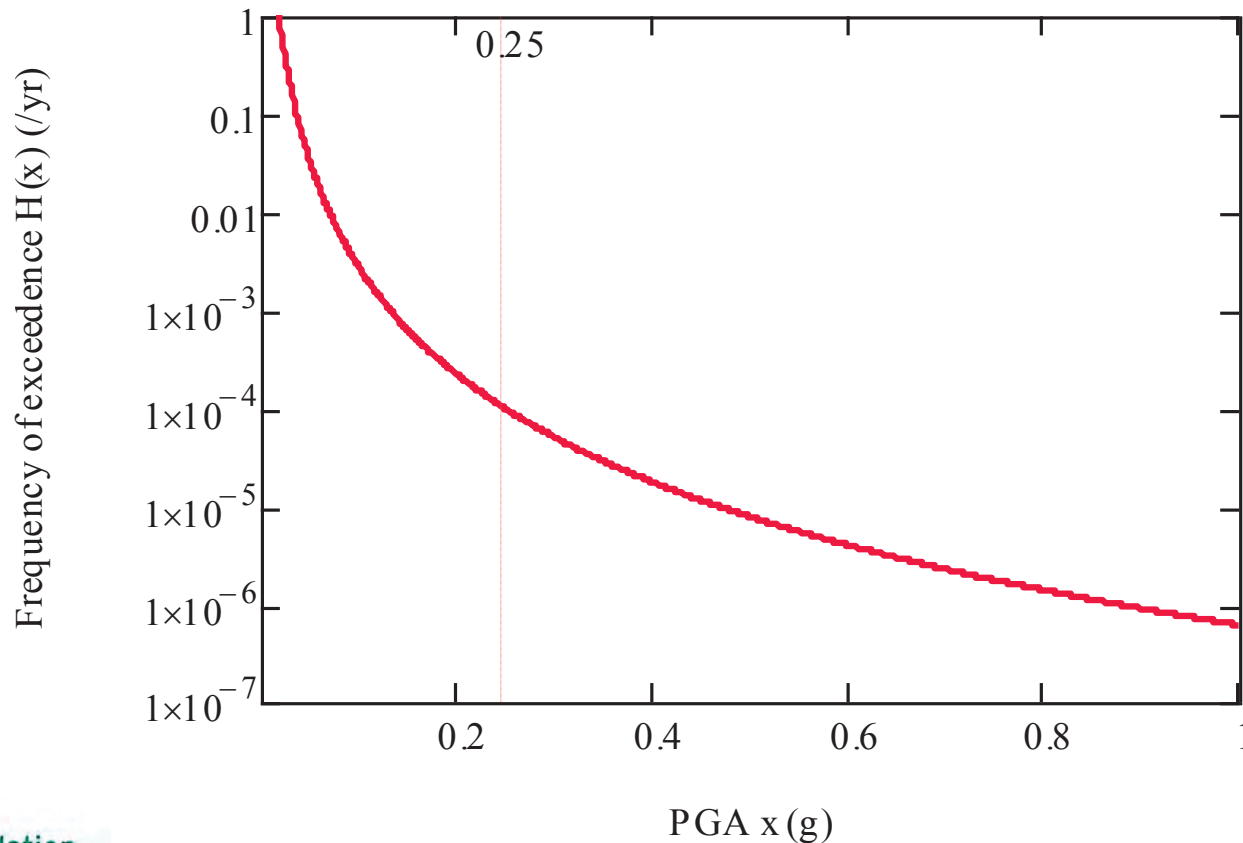
- Need to define hazard initiated faults and their sequences of plant failures
 - Normal to neglect explicit representation of dose consequences
- Assume fault is protected by one or more Lines of Protection (LoP)
- Need probabilistic (or frequency) hazard and fragility functions
- Hazard functions are simple inverse decreasing curves
 - But defining equations are complex
- Nuclear plant fragilities have only been developed in detail for seismic hazard
 - Fukushima event has prompted research into fragilities for other natural hazards

Simple seismic risk example – seismic hazard

- Hazard model: Kennedy Power Law model: $H(0.25g) = 10^{-4}/\text{yr}$

$$H(x) = 6.113 \cdot 10^{-7} \cdot x^{-3.677}$$

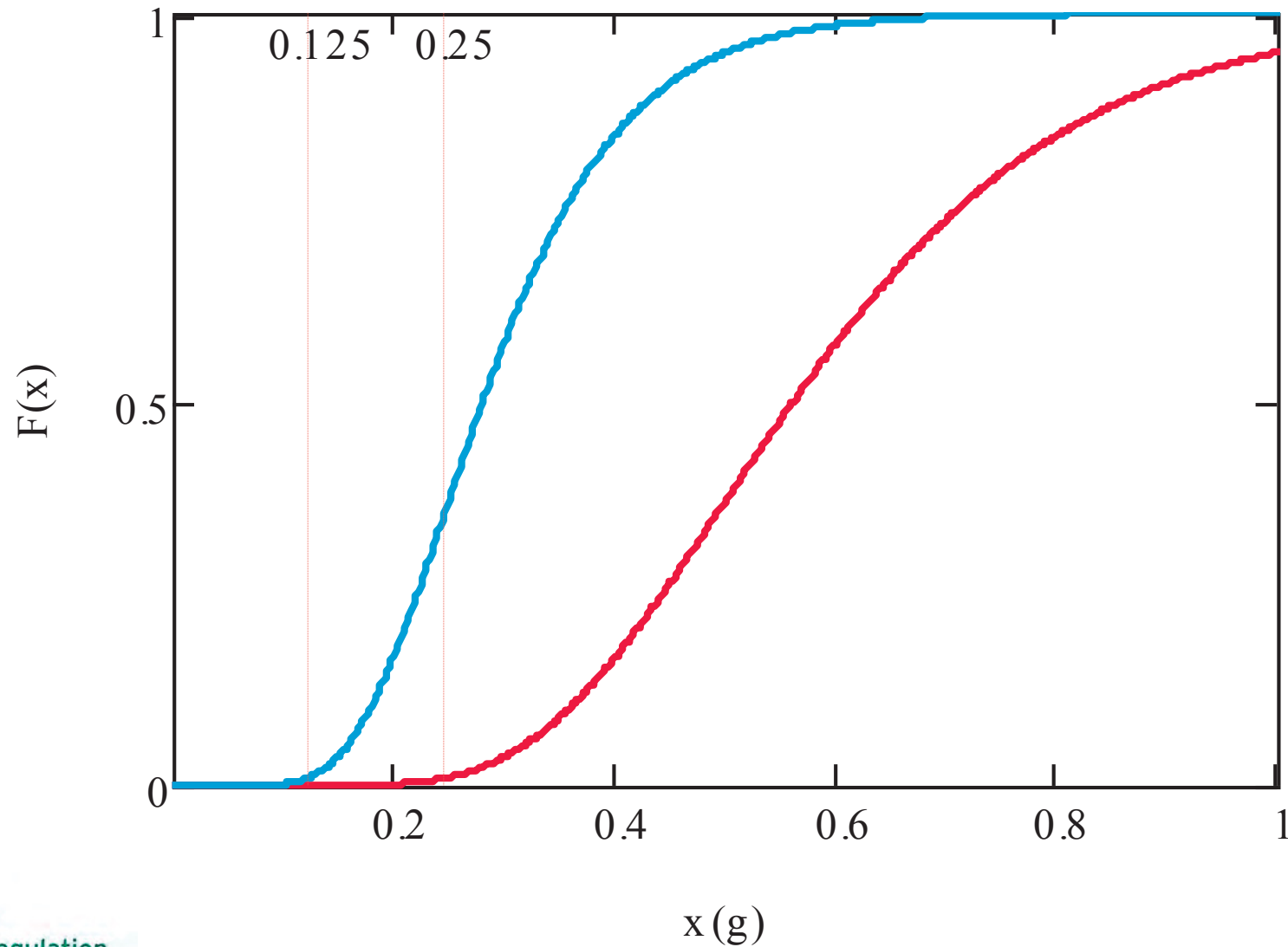
- Note: this is a frequency of exceedance model



Seismic fragility model

- Fragility model: Lognormal single uncertainty parameter model
 - Note: This is a **probability model**
 - Applies to a given fault, mitigated by a LoP with known mode of failure
 - Needs only 2 parameters to define for each LoP
 - Median x & log. standard deviation β
- ***This is a simplified model compared to those normally used in seismic PSA***

Seismic fragility curves



Seismic design basis and High Confidence of Low Probability of Failure (HCLPF)

- For single param. uncertainty fragility model: $HCLPF \approx X_{1\%}$
- Set Design Basis (DB) to this value: $X_{DB} = X_{1\%}$
- Representative plant data assumed as below

Line of protection	$X_{1\%} = X_{DB}$	β	Median x	$H(X_{DB})$
A	0.25g	0.35	0.565	$10^{-4}/\text{yr}$
B	0.125g	0.35	0.283	$1.3 \times 10^{-3}/\text{yr}$

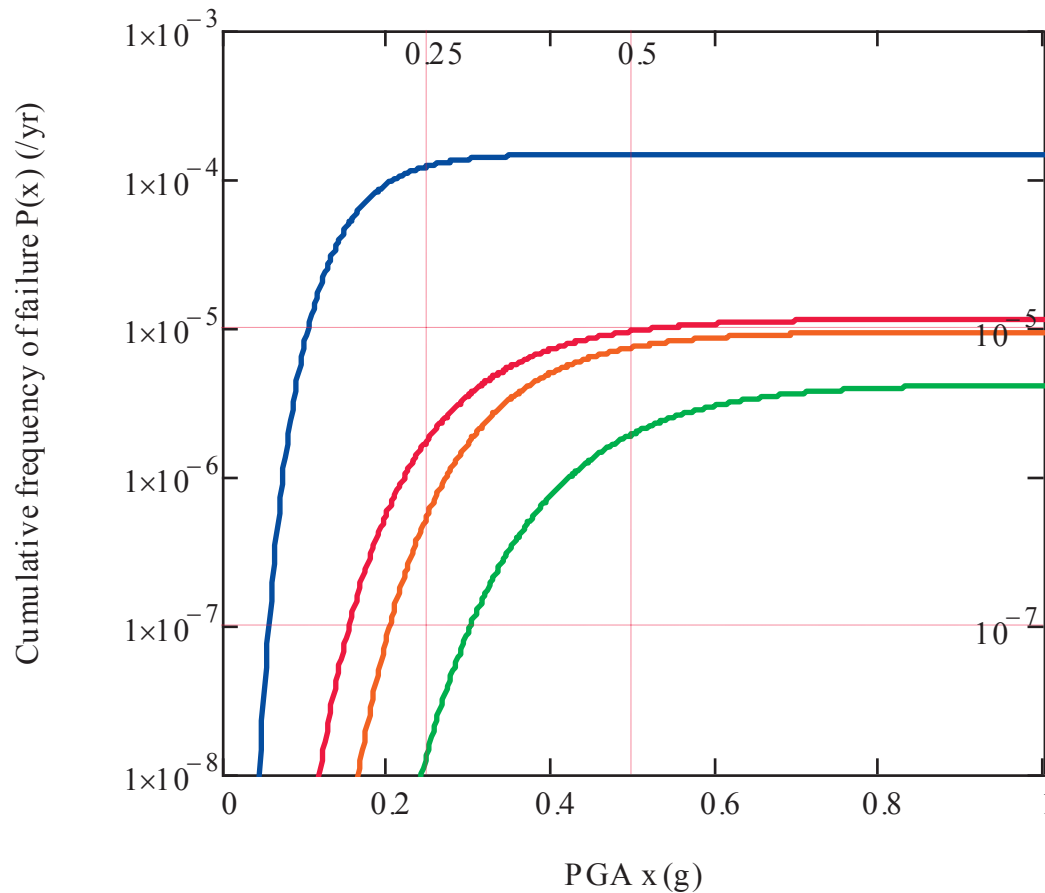
Seismic risk model

- Risk Model: Standard model derived from reliability theory
 - Calculates $P(\infty)$: Frequency of plant failure for given fault

$$P(\infty) = \int_0^{\infty} H(x) \cdot f(x) \cdot dx = \int_0^{\infty} h(x) \cdot F(x) \cdot dx$$

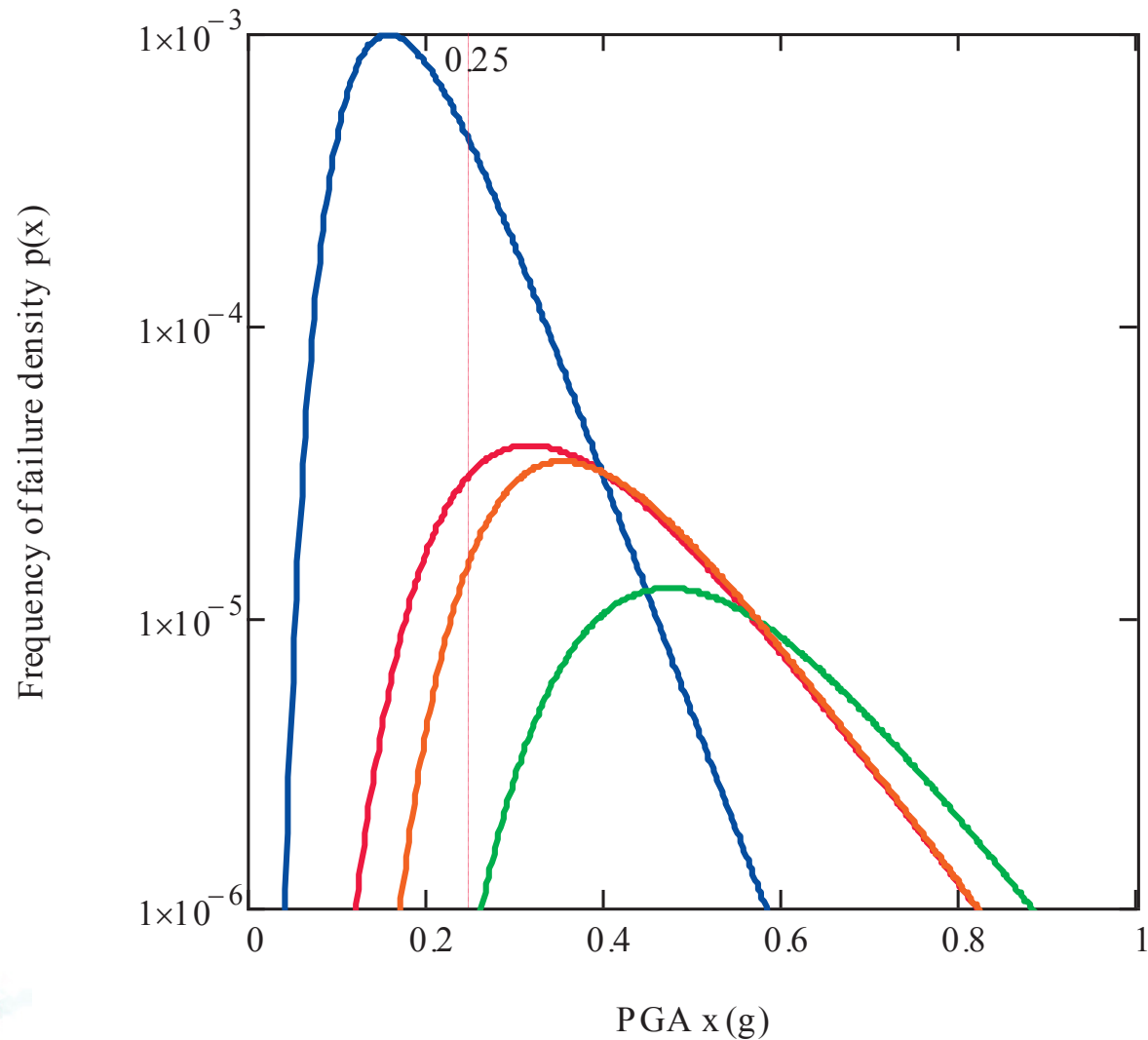
Risk results #1

$P_A(\infty)$	$P_B(\infty)$	$P_{A \cap A}(\infty)$	$P_{A \cap B}(\infty)$
$1.1 \times 10^{-5}/\text{yr}$	$1.5 \times 10^{-4}/\text{yr}$	$4.1 \times 10^{-6}/\text{yr}$	$9.4 \times 10^{-6}/\text{yr}$



Risk results #2

- Most of the risk arises at just beyond the Design Basis



Deductions – Single LoP & effect of hazard curve

- Line A alone:
 - Gives about an order of magnitude of protection over the DB exceedance frequency.
 - Note: for exceedance frequency (and prob.) hazard curves
 - ($10^{-4}/\text{yr}$ design basis) x (10^{-2} failure per demand) \neq ($10^{-6}/\text{yr}$ plant failure frequency)
 - Most of the failure frequency occurs just beyond the design basis
 - Saturates at about twice $X_{DB} \sim 0.5g$, or 2 x DB or $\sim 10^{-5}/\text{yr}$
 - Therefore: BDB value should be $\sim 10^{-5}/\text{yr}$
- Line B alone:
 - Same applies but significantly worse – as expected

Deductions – Two LoP & common-cause effect

- Lines $A \cap A$:
 - Adding a second independent LoP of equal reliability reduces $P(\infty)$ by factor of ~ 2.7 to $4 \cdot 10^{-6}/\text{yr}$
 - **NOT: $P_A \times P_A \sim 10^{-5} \times 10^{-5} \sim 10^{-10}/\text{yr}$**
 - This is due to **common-cause** nature of hazard
- Lines $A \cap B$:
 - Adding a second independent LoP of significantly lower reliability provides very little improvement to overall plant failure frequency
 - This is because the **common-cause** nature of the hazard affects both LoPs and advantage from Line B fades to ~ 0 by 0.25g

Saturation risk and overall plant risk

- **At $10^{-5}/y$:** hazard subject to increasingly large uncertainties
 - Majority of failure frequency accrued by $10^{-5}/yr$ hazard level
 - Useful BDB region for natural hazards is $10^{-4}/yr \rightarrow 10^{-5}/yr$
- **Beyond $10^{-5}/yr$:** increasingly approaching *Severe Accident* territory
- Target 8, large release for single class of hazard BSO is $10^{-7}/yr$
 - Overall station risk $\sim 10^{-6}/yr$ for new builds
- Very large uncertainties in hazard analyses at these very low exceedance probabilities
 - **Precautionary Approach** - Can major release occur at these very low probability hazard levels?
 - Seismic hazard in UK \rightarrow max. up to $\sim 1g!$
 - If so, hazard could dominate overall station risk

Final thought!

- An enigmatic quote from two anthropologists on society's approach to risk:

“Can we know the risks we face, now or in the future? No, we cannot; but yes we must act as if we do.”

From: Douglas & Wildavsky, Risk and Culture (1982)

- Thank you